



SAVADESIGN d.o.o., projektovanje i konsalting
M. Mitrovica 22202
A. L. Stankovića 46
www.savadesign.net
gbudecevic@savadesign.net

Objekat: Čamac – Hunter 575
Predmet: Hidrostatički proračun i proračun stabiliteta
Investitor: Nautikcentar, SRBIJA
Dostaviti: Nautikcentar, SRBIJA

ČAMAC HUNTER 575 -HIDROSTATIKA&PRORAČUN STABILITETA-

u Mačvanskoj Mitrovici
17.09.2013. god.

Sastavio:
Goran Budečević, dipl.ing.



1. Opšte

Za čamac Hunter 575, hidrostatički proračuni i proračun stabiliteta je urađen. Glavne karakteristike čamca date su u tekstu dole.

2. Osnovne karakteristike

Osnovne karakteristike date su u tekstu dole:

LH	5.75	m	length
BH	1.72	m	breadth
D ₀	280	kg	mlcc light craft displacement
T ₀	0.08	m	light craft displacement coresponding draft crew
CL	6		limit mass of desired crew
m _{CL}	450	kg	crew
m _{provision}	30	kg	provision
m _{fuel}	25	kg	fuel
m _{fittings}	180	kg	fittings and engine for 60 HP
m _{mtl}	685	kg	maximum total load
m _{lcc}	280	kg	light craft condition mass
m _{ldc}	965	kg	loaded displacement mass
T ₁	0.195	m	loaded displacement mass coresponding draft

3. Hidrostatički proračun

Rezultati hidrostatičkih proračuna dati su u tekstu dole.

Displacement t	0	0.1282	0.3884	0.9979	1.675	2.401
Draft	0	0.05	0.1	0.2	0.3	0.4
WL Length m	1.622	4.422	4.757	5.11	5.318	5.49
Beam max extents on WL m	0	1.372	1.434	1.474	1.515	1.557
Wetted Area m ²	0	4.589	6.015	7.519	8.887	10.12
Waterpl. Area m ²	0	4.518	5.616	6.477	7.025	7.495
Block coeff. (Cb)	0	0.422	0.569	0.662	0.693	0.702
Max Sect. area coeff. (Cm)		0.83	0.884	0.869	0.893	0.899
Waterpl. area coeff. (Cwp)	0	0.745	0.823	0.86	0.872	0.877
LCB from zero pt. (+ve fwd) m	2.813	1.667	1.882	2.105	2.222	2.303
LCF from zero pt. (+ve fwd) m	2.768	1.823	2.111	2.333	2.445	2.527
KB m	0	0.032	0.061	0.116	0.171	0.225
BMt m	0.001	4.542	2.179	1.039	0.703	0.547
BML m	11973.9	38.389	20.106	11.264	8.191	6.66
KMt m	0.001	4.575	2.241	1.155	0.874	0.772
KML m	11973.9	38.422	20.167	11.38	8.362	6.885
Immersion (TPc) tonne/cm	0	0.045	0.056	0.065	0.07	0.075

4. Proračun centracije

Rezultati proračuna centracije dati su u tekstu dole.

Weight calculation

	mass	Zg	Mz
	(kg)	(m)	(kg.m)
m _{lcc}	180	0.2	36
m _{provision}	30	0.1	3
m _{fuel}	25	0.2	5
m _{fittings}	140	0.2	28
m _{CL}	300	0.4	120
m _{ldc}	675		192

ZG1 0.2844 m vertical center of gravity

Weight calculation

	mass	Zg	Mz
	(kg)	(m)	(kg.m)
m _{lcc}	180	0.2	36
m _{provision}	30	0.1	3
m _{fuel}	25	0.2	5
m _{fittings}	140	0.2	28
m _{CL}	300	0.4	120
m _{ldc}	675		192

ZG1 0.2844 m vertical center of gravity

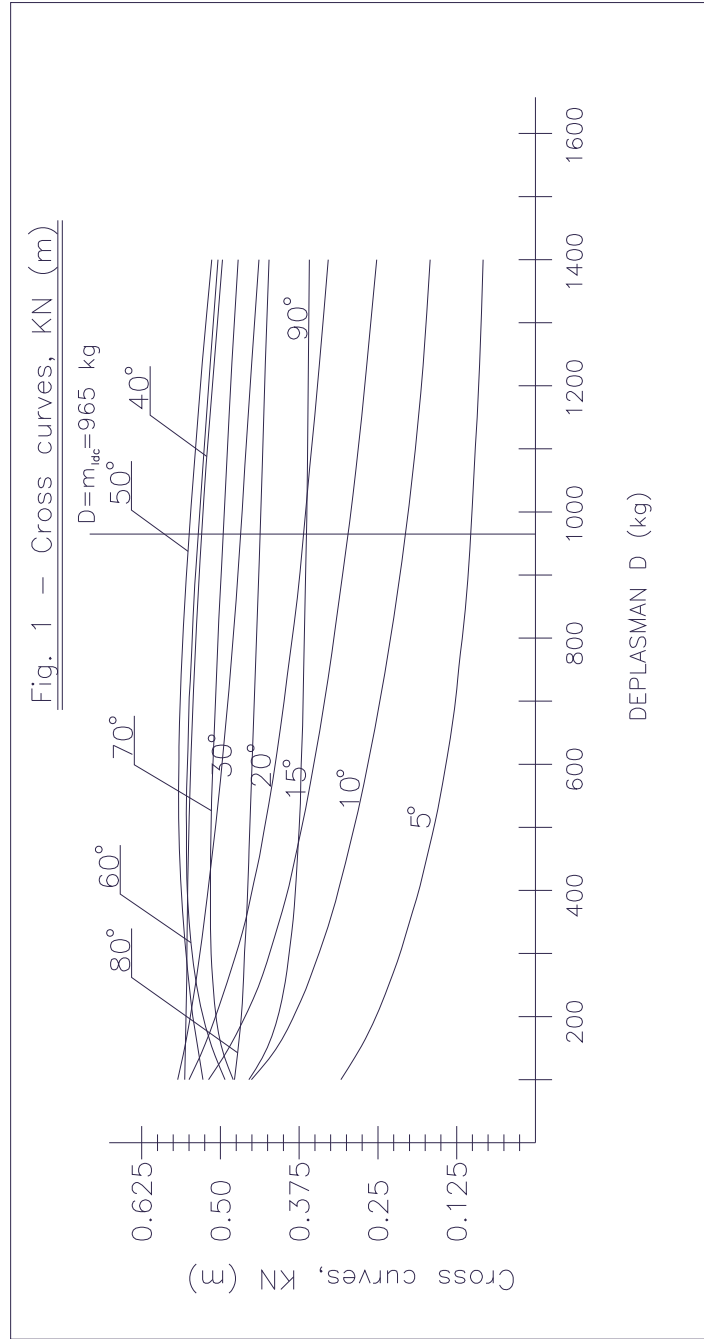
5. *Poprečne krive stabiliteta, KN*

Rezultati proračuna dati su u tekstu dole.

		cross curves, KN (m)				
		heeling angle φ (°)				
	0	5	10	15	20	30
0.1	0	0.309	0.451	0.519	0.55	0.568
0.15	0	0.278	0.411	0.487	0.527	0.557
0.2	0	0.253	0.384	0.461	0.508	0.548
0.25	0	0.233	0.362	0.439	0.491	0.54
0.3	0	0.215	0.344	0.422	0.475	0.533
0.35	0	0.2	0.327	0.407	0.461	0.526
0.4	0	0.185	0.313	0.393	0.45	0.52
0.45	0	0.173	0.3	0.382	0.439	0.514
0.5	0	0.161	0.288	0.371	0.43	0.508
0.55	0	0.151	0.276	0.361	0.421	0.503
0.6	0	0.142	0.266	0.352	0.413	0.498
0.65	0	0.134	0.256	0.343	0.406	0.493
0.7	0	0.127	0.247	0.335	0.399	0.488
0.75	0	0.122	0.238	0.327	0.393	0.484
0.8	0	0.116	0.23	0.32	0.386	0.48
1	0	0.101	0.202	0.293	0.365	0.466
1.2	0	0.09	0.181	0.271	0.346	0.453
1.4	0	0.083	0.167	0.252	0.329	0.439

		cross curves, KN (m)				
		heeling angle φ (°)				
	40	50	60	70	80	90
0.1	0.557	0.528	0.493	0.48	0.478	0.455
0.15	0.556	0.536	0.513	0.498	0.472	0.426
0.2	0.555	0.544	0.528	0.507	0.467	0.409
0.25	0.554	0.55	0.538	0.512	0.464	0.398
0.3	0.553	0.555	0.545	0.515	0.462	0.391
0.35	0.553	0.559	0.55	0.516	0.459	0.385
0.4	0.552	0.562	0.553	0.516	0.457	0.381
0.45	0.551	0.565	0.554	0.516	0.455	0.378
0.5	0.55	0.566	0.554	0.515	0.454	0.375
0.55	0.549	0.567	0.554	0.514	0.452	0.373
0.6	0.547	0.566	0.553	0.512	0.45	0.372
0.65	0.546	0.566	0.551	0.51	0.448	0.37
0.7	0.544	0.564	0.55	0.508	0.446	0.369
0.75	0.542	0.562	0.547	0.506	0.445	0.368
0.8	0.539	0.56	0.545	0.504	0.443	0.367
1	0.528	0.547	0.533	0.494	0.436	0.363
1.2	0.513	0.532	0.519	0.484	0.43	0.361
1.4	0.497	0.514	0.504	0.472	0.423	0.359

Rezultati su prikazani i u formi dijagrama:



6. Proračun stabiliteta

Rezultati proračuna dati su u tekstu dole:

φ	$\sin\varphi$	φ (rad)	KN	KG	GZ	M1G1	D1	Mst
0	-	0	-	0.2902	-	-	965	0
5	0.087	0.087266	0.08	0.2902	0.103	0.8888	965	99.395
10	0.174	0.174533	0.161	0.2902	0.206	0.8888	965	198.790
15	0.259	0.261799	0.244	0.2902	0.298	0.8888	965	287.570
20	0.342	0.349066	0.309	0.2902	0.368	0.8888	965	355.120
30	0.5	0.523599	0.394	0.2902	0.468	0.8888	965	451.620
40	0.643	0.698132	0.425	0.2902	0.53	0.8888	965	511.450
50	0.766	0.872665	0.423	0.2902	0.55	0.8888	965	530.750
60	0.866	1.047198	0.399	0.2902	0.535	0.8888	965	516.275
70	0.939	1.22173	0.36	0.2902	0.496	0.8888	965	478.640
80	0.985	1.396263	0.308	0.2902	0.438	0.8888	965	422.670

Gde je:

KN -	Položaj tež. Istisnuća za odgovarajući ugao nakretanja, m
KG-	Položaj težišta po visini, Zg, m
GZ-	Krak stabiliteta, m
M1G1-	Metacentarska visina, m
D1-	Maksimalni deplasman, kg
Mst-	Moment stabiliteta, kg.m

Analiza je urađena u skladu sa pravilima Lloyd Registrar; Special Service Craft Rules. za slučaj stabiliteta u neoštećenom stanju. Rezultati su prikazani u tekstu dole:

General intact stability criteria

- 1 The area under GZ curve is not to be less 0.055 m.rad. up to $\phi=30^\circ$
0.1570 YES
- 2 The area under GZ curve is not to be less 0.09 m.rad. up to $\phi=40^\circ$
0.189943 YES
- 3 The area under GZ curve between $\phi=30^\circ-40^\circ$ is not to be less 0.03 rad.m.
0.0329 YES
 The righting lever GZ is to be at least 0.20 m at angle of heel to or greater than
- 4 30°
FOR $\phi=30^\circ$ GZ=0.468 m YES
 The max. GZ is to occur at an angle of heel preferably exceeding $\phi=30^\circ$ but not less than
- 5 $\phi=25^\circ$.
GZ max.is for $\phi=50.5^\circ$ YES
- 6 The initial metacentric height M1G1 is to be not less than 0.15 m
M1G1= 0.8888 m YES
 The angle of heel on account of crowding of guests to one side is not to exceed
- 7 10°
Mnp = 483 kg.m > M($\phi=10^\circ$)=200 kg.m, NO, FB = 207 mm
 The angle of heel on account of turning is not to exceed
- 8 10°
 when the heeling moment determined by the following formula is applied:

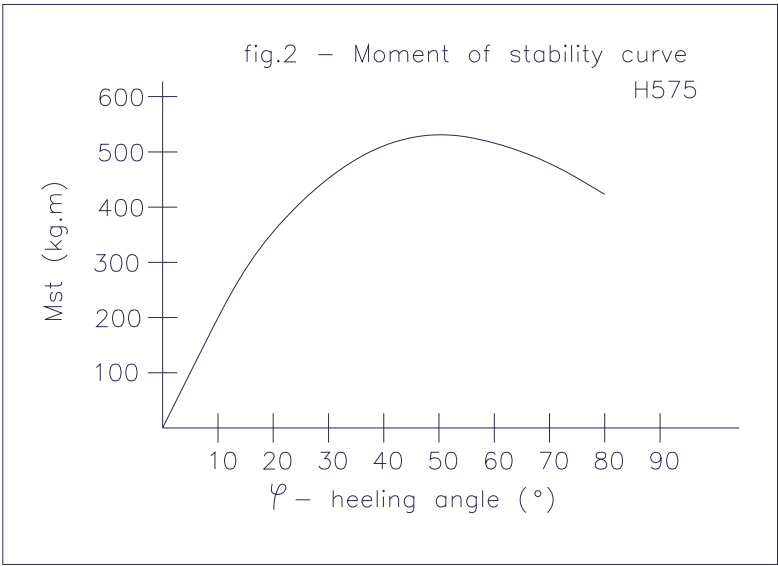
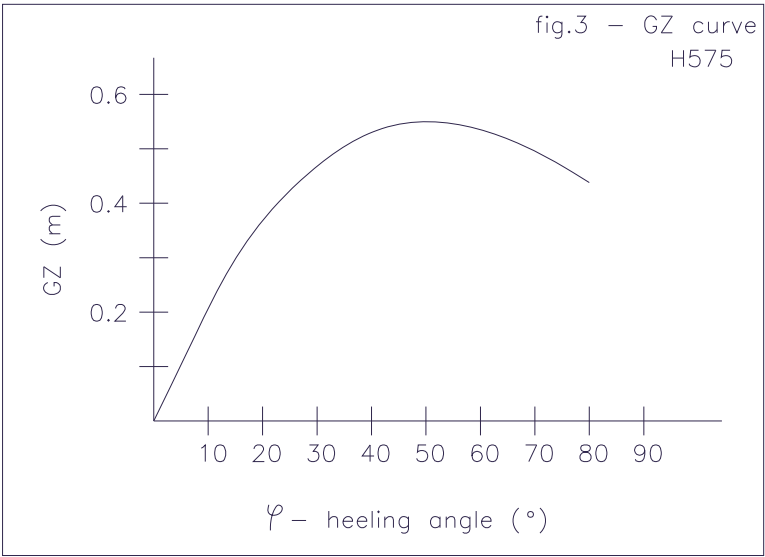
$$M_H = \frac{(0.02 * V_o^2 * \Delta * (KG - 0.5 * T_m))}{L_{wl}}$$

V_o – service speed(m/s),
 Δ – displacement (t),
 KG – height of centre of gravity above keel(m),
 T_m – mean draught (m),
 L_{wl} – waterline length (m).
 M_H -heeling moment (t.m)

V_o	16	29.632	8.23	m/s
Δ	0.965	t		
KG	0.290155	m		
T_m	0.195	m		
L_{wl}	4.836	m		

M_H 52.09178 kg.m

Mh =52.1 kg.m < M($\phi=10^\circ$)=200 kg.m YES



7. Zaključak

Prethodna analiza, kao i mnogo godina prakse, pokazala je dobre karakteristike stabilneta prema LR SSC Rules kriterijumima, osim u slučaju prelaska svih putnika na jedan bok kada ugao prelazi 10° ali je visina slobodnog boka i dalje zadovoljavajuća (207 mm). Postojanje krivih stabilneta, proračun stabilneta po bilo kojim drugim kriterijumima čini relativno lakim. Ipak, finalni zaključak o stabilnetu čamca daće nadležna ustanova.